

**CANTILEVER TIMBER COLUMN SELECTION TABLE**

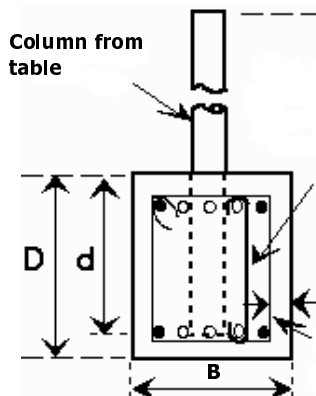
**WITH LATERAL LOAD APPLIED AT TOP**

California Building Code 2007 Edition (CBC), NDS 2005

DESIGN CRITERIA (Based on Working Stress Design Method):

Concrete  $f'_c = 2500$  psi

Timber posts: Basic Stresses from Plate B-5 + 1/3 increase included. Maximum deflection (using  $e_{MIN} = L / 200$ )



**CROSS-SECTION**

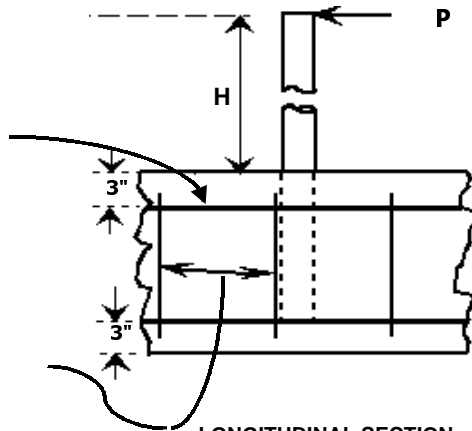
Reinforcement from table at both top and bottom. Space bars uniformly. When an odd number of bars are used at top and bottom, bend center bar 90° around column from each side.

When interior bars are more than 6" from an adjacent longitudinal bar, provide #3 Ties @ 12" o.c.

3" Typ

Provide #3 Ties @ 12" o.c. throughout, around the outside longitudinal bars.

Load "P" is applied to the stronger axis of the column.



**LONGITUDINAL SECTION**

DOUGLAS FIR SIZE - GRADE		H = COLUMN HEIGHTS IN FEET										GRADE BEAM		
		7	8	9	10	11	12	13	14	15	B	D	d	
		MAXIMUM P IN POUNDS (Governed by Deflection = L / 200)												
4 x 6 - #2	P	59	45	36	29	24	20	17	14	13	12	12	9	
	Min $A_s$	0.042	0.036	0.033	0.029	0.027	0.024	0.022	0.020	0.020				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
4 x 6 - #1	P	63	48	38	31	25	21	18	15	13	12	12	9	
	Min $A_s$	0.045	0.039	0.035	0.031	0.028	0.025	0.024	0.021	0.020				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
4 x 6 - #1+	P	68	52	41	33	27	23	19	17	14	12	12	9	
	Min $A_s$	0.048	0.042	0.037	0.033	0.030	0.028	0.025	0.024	0.021				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
4 x 6 - SS	P	71	54	43	34	28	24	20	17	15	12	12	9	
	Min $A_s$	0.050	0.044	0.039	0.034	0.031	0.029	0.026	0.024	0.023				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
6 x 6 - #2	P	76	58	46	37	30	25	22	19	16	12	12	9	
	Min $A_s$	0.054	0.047	0.042	0.037	0.033	0.030	0.029	0.027	0.024				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
6 x 6 - #1	P	94	71	56	46	38	31	27	23	20	12	12	9	
	Min $A_s$	0.066	0.057	0.051	0.046	0.042	0.038	0.035	0.033	0.030				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
6 x 6 - SS	P	94	71	56	46	38	31	27	23	20	12	12	9	
	Min $A_s$	0.066	0.057	0.051	0.046	0.042	0.038	0.035	0.033	0.030				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
6 x 8 - #2	P	193	147	116	94	78	65	56	48	42	18	15	12	
	Min $A_s$	0.102	0.089	0.079	0.071	0.065	0.059	0.055	0.051	0.048				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
6 x 8 - #1	P	238	182	144	116	96	81	69	59	51	18	15	12	
	Min $A_s$	0.126	0.110	0.098	0.088	0.080	0.074	0.068	0.063	0.058				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
6 x 8 - SS	P	238	182	144	116	96	81	69	59	51	18	15	12	
	Min $A_s$	0.126	0.110	0.098	0.088	0.080	0.074	0.068	0.063	0.058				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
8 x 8 - #2	P	263	201	159	129	106	89	76	65	57	18	15	12	
	Min $A_s$	0.139	0.122	0.108	0.098	0.088	0.081	0.075	0.069	0.065				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
8 x 8 - #1	P	325	248	196	159	131	110	94	81	70	18	15	12	
	Min $A_s$	0.172	0.150	0.134	0.120	0.109	0.100	0.093	0.086	0.080				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
8 x 8 - SS	P	325	248	196	159	131	110	94	81	70	18	15	12	
	Min $A_s$	0.172	0.150	0.134	0.120	0.109	0.100	0.093	0.086	0.080				
	Re-Bars	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
8 x 10 - #2	P	535	409	323	262	216	182	155	133	116	18	15	12	
	Min $A_s$	0.284	0.248	0.220	0.198	0.180	0.165	0.153	0.141	0.132				
	Re-Bars	2-#4	2-#4	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3	2-#3				
8 x 10 - #1	P	660	505	399	323	267	224	191	165	143	18	15	12	
	Min $A_s$	0.350	0.306	0.272	0.245	0.222	0.204	0.188	0.175	0.162				
	Re-Bars	2-#4	2-#4	2-#4	2-#4	2-#3	2-#3	2-#3	2-#3	2-#3				
8 x 10 - SS	P	660	505	399	323	267	224	191	165	143	18	15	12	
	Min $A_s$	0.350	0.306	0.272	0.245	0.222	0.204	0.188	0.175	0.162				
	Re-Bars	2-#4	2-#4	2-#4	2-#4	2-#3	2-#3	2-#3	2-#3	2-#3				

**DIVISION OF BUILDING AND SAFETY**

**COUNTY OF VENTURA**

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BUILDING OFFICIAL \_\_\_\_\_

B & S STD

**B-38**

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